Digital BCM Receiver Yury Kolomensky **UC Berkeley/LBNL** 06-May-23

On behalf of: Yuan Mei Shuije Li, John Arrington, Ernst Sichtermann





Beam Instrumentation Challenge

Requirements on the beam asymmetry: Δx or $A_Q = (Q_R - Q_L)/(Q_L + Q_R)$

Parameter	Jitter requirement	Achieved	Resolution requirement	Achieved
Charge	< 1000 ppm	$500 \mathrm{~ppm}$	< 10 ppm	$65 \mathrm{~ppm}$
Energy	<pre>108 ppm</pre>	$6.5 \mathrm{~ppm}$		
Position	$< 47 \ \mu m$	$48~\mu{ m m}$	$< 3 \ \mu { m m}$	$2.4~\mu{ m m}$
Angle	$< 4.7 \ \mu rad$	$1.4 \ \mu rad$		

Source: MOLLER CDR. Requirements quoted for 1920 Hz helicity flip rate LBNL direct-sampling RF receiver is designed to satisfy the requirements on the beam charge resolution Development of a direct-sampling RF receiver for precision beam charge measurements in the MOLLER experiment

> Y. Mei¹, S. Li¹, J. Arrington¹, J. Camilleri¹, A. Cuda², J. Egelhoff², Yu.G. Kolomensky^{1,2} and E.P. Sichtermann¹

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System architecture: digital RF receiver



- High sampling rate (>~3Gsps) and high dynamic range (>10bits) ADCs that are capable of direct RF sampling
- Amplitude fluctuation of LO doesn't contribute. Phase noise is small; modest contribution to the final uncertainty
- Filtering and decimation done digitally in ADC and/or FPGA
- Output: decimated data stream, integrated in 0.5 msec windows in FPGA or offline
- Implemented in a 4-channel prototype receiver box





4 RF channels

Single channel chain

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Figure 3. The RF front-end signal processing chain of the sampling system with the part numbers.



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VCU108 FPGA board ADC32RF45EVM Amplifier and filter

Directional coupler

Beam Test in Hall A in Sept 2020 (CREX)



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Input: 1497 MHz RF signal

1. Direct sampling at 3072 Msps (14-bit, 10-bit ENOB)

 $x_i = A\cos(2\pi f_0\theta_i)$

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where
$$f_0 = 1497$$
 MHz, $fs_0 = 3072$ MHz, $\theta_i = \frac{i}{fs_0}$

2. Digital Down Conversion (DDC) with tunable (numerical) LO

$$I_i = x_i \cos(2\pi f_1 \theta_i + \phi), Q_i = x_i \sin(2\pi f_1 \theta_i + \phi).$$

$$y_i = I_i + \mathbf{j}Q_i, \text{ two freq. } f_0 + f_1 \text{ and } f_0 - f_1.$$

filtered out

3. /16 decimation: keep 1 sample every 16 samples (selectable between 4-32)

 $fs = fs_0/16 = 192 \text{ MHz}$

Final data stream: I/Q (16-bit each) at **192** Msps rate (\sim 2 x 400 MB/s)







Define resolution as double-difference (ddf): $ddf = (A_A - A_B)/\sqrt{2}$



σ_{ddf} (/

Bench test with beam generator: 8 ppm @ 2 kHz helicity rate

Beam test with cavity signals: 25 ppm @ 2 kHz helicity rate

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Potential sources of Beam Noise



Additional ~ 20 ppm of beam-induced noise; appears to scale as 1/f Not seen (?) in CREX at ~120 Hz, but see caveats below



Potential sources of noise

- Large beam jitter (in particular position) during transition between the helicity windows
 - We did not sync to the helicity windows and we integrate over these transitions
 - If this is the source, it would be (fairly easily, FLW) handled by feeding the helicity signal into our data stream (needs to be done for MOLLER anyway)
 - Not clear though why it scales as 1/f
- Systematics in the BCM-based measurement?
 - Halo and other losses between cavities that could scale as I/f
 - Phase and tune drifts ? also scales as 1/f.
 - Tested cables on the bench at LBNL but not in situ did not see a smoking gun

Position dependence of BCM signal LER





To contribute to asymmetry, requires

- cavity mis-alignment, and
- time-dependent beam position 2.
 - beam position fluctuation a.
 - b. raster

Implies requirement on relative alignment of the cavity electrical centers to ~1mm or regression of BCM signal against BPM signals

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- There is nontrivial beam structure around the 1497 MHz carrier frequency: AMmodulated intensity
 - Time multiplexing beam signals at ~1 MHz is dangerous and should be avoided
 - In discussion with JLab beam instrumentation group to remove mux from the JLab BCM readout (written in requirements document)
- Important to integrate BCM signals over the correct helicity windows
- Being able to regress/correct against beam position would be useful



Figure 8. Power spectrum of a representative cavity signal induced by 130 µA beam. NCO is set to 1485 MHz and is digitally mixed with the input and then decimated by a factor of 16, resulting in an effective sampling rate of 192 MHz. The 1497 MHz input signal appears as two mixing product peaks marked 1 and 2 at 12 MHz and 90 MHz, respectively. Both I and Q are recorded and combined to compute the power spectrum via complex-input FFT, as shown in the left panel. The right panel shows a zoomed-in view around peak 1, which is of primary interest.

WILLER Implementation in MOLLER

- Would ideally upgrade from NI digitizer+Xilinx FPGA to an integrated Xilinx Zynq RFSoC (e.g. ZU48DR on a ZCU208 eval board)
 - 8 channels @ 5 GSPS, 14 bits: sufficient specs
 - FMC mezzanine slot, e.g. for helicity sync
 - ARM processor can run an instance of CODA
 - Similar architecture to the TRIUMF digitizers: can share firmware/software
 - Would need I module for BCMs, 2 if include BPMs
- Alternative is to duplicate our existing 4-channel box to read out 5 BCMs (and possibly 6 BPMs)
 - Would need I-2 additional boxes
 - Helicity sync and DAQ interface more complicated
- Need to plan commissioning/beam tests carefully



Implementation in MOLLER



- - Could instrument all or some: absolute minimum would be 2 BCMs
- Ideally would amplify the signals in the Hall A labyrinth
- Ideally would retune BCMs for higher Q

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Progress Since 2022

- No funding at Berkeley for this work have to scavenge for resources
- Procured RFSoC 4x2 kit (RFSoC-PYNQ) to test functionality
 - A student brought it up, measured amplitude and phase noise — seems adequate
 - Developments synergistic with my other projects (and Aled is working with this board at UCSB) — can make some progress without MOLLER-specific funds
 - Incoming Berkeley graduate student interested in MOLLER will (hopefully) start working with this system in the Fall
- Ultimately, if MOLLER is interested in this technology, we'll need to find a way to pay for the development

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- Internal noise (8 ppm) of the digital BCM processor satisfies MOLLER specs, could be further improved
- Noise performance in the beam test not (quite) up to spec; needs to be understood
- Need implementation and deployment/commissioning plan
- Started discussions with the DAQ group about integration with the DAQ
 - Ideally, BCM processor would look very similar to the MOLLER digitizers with the new Zyng RFSoC







Noise Budget

- Noise budget/requirements for $\sigma_Q/Q < 14$ ppm: assume fs=3 GHz and $\Delta T=0.5$ msec
- Digitizer (white) noise $\underbrace{\sigma_Q}_{O} = 2^{-\text{ENOB}+3/2} \cdot \frac{1}{\sqrt{f_c \Delta T}} \rightarrow \text{ENOB} > 8 \text{ bits}$
- Thermal noise: -124 dB @ 2 kHz for beam signal of -18 dBm $\rightarrow \sigma_0/Q \sim 0.6$ ppm
- Phase noise (uncorrelated time jitter, though mindful of 1/f contributions):

$$\frac{\sigma_Q}{Q} \sim \frac{\pi f \sigma_t}{\sqrt{f_s \Delta T}} \rightarrow \sigma_t < 3.6 \text{ psec}$$

- Simulation by Joe Camilleri: $\sigma_t < \sim 1$ psec
- Spec of $\sigma_0/Q < 14$ ppm achievable with currently available hardware

LER **BCM** Digital Receiver Prototype

- LDRD at LBNL
 - FY18: prototyping, bench tests
 - FY19: full hardware/firmware implementation, beam tests
- Prototype based in TIADC32RF45 evaluation board and ADC capture card; stream raw data to disk $(\sim 200 \text{ msec} \rightarrow 2 \text{ GB})$
 - 14-bit ADC but limited to 12 bits by JESD204B interface with capture card
- Offline analysis (DDC, averaging, asymmetry analysis)



Joe Camillieri

digital BCM



- ERA Instruments ERASynth+: software-configurable, low-jitter RF generator; oven-controlled oscillator
- Use two phase-locked generators
 - 3 GHz clock
 - RF signal (<1.5 GHz)
 - Split signal between 2 input channels of the ADC (typically 9 dBm/channel)



Phase Noise Start 100 Hz

Phase Noise: Hold Cor Ctrl OV Pow OV Attn OdB ExtRef1 ExtRef2 Stop Svc 2018-04-13 16:15

Stop 5 MHz

LER RF clock: phase noise

Adequate for 10 ppm resolution



Figure 27: ERASynth+ Phase Noise Performance at 3 GHz RF Output

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James Egelhoff

I kHz pairs I497 MHz, +9 dBm input signal per channel 3000 Msps, I2 bit digitizer







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James Egelhoff

LER Systematics: phase drifts

Quadrature sum of I/Q demodulated signals is relatively insensitive to slow phase drifts

$$A = \sqrt{I^2 + Q^2}$$

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- at the cost of 3 dB increase in noise
- Slow phase drifts with f<500 Hz cancel out to good precision in helicity quads
- Will simulate residual sensitivity to drifts of the cable delay (phase drift) and drifts of the cavity frequency
- Will develop firmware to monitor/calibrate cavity frequency
- If necessary, can deploy phase stabilization hardware developed for LCLS-II

Potential Systematics: beam phase jitter

- Cavity BCMs introduce one potential systematics into the measurement of charge: they do not measure beam charge directly
- Signal induced by each bunch is a projection of the its phasor onto the EM field phasor of the cavity, i.e.

 $\mathbf{E}_c \cdot \mathbf{E}_h \propto q_h \cos \Delta \phi$

- Naive calculation: assume that the phase shift is *uncorrelated* bunch-to-bunch, i.e. it is dominated by white noise
- Then $\sigma_Q/Q < 14$ ppm \rightarrow to $\sigma_{\omega} < 0.1$ rad for bunch frequency of 250 MHz and 0.5 msec

the right

Such jitter seems unlikely: beam energy spread is $\sim \sigma_{\varphi} \sin \varphi_{acc}$, and σ_{E} of a few percent seems large

However, correlated phase shifts could be a problem (correlates energy spread and charge error from cavity BCM)





Do We Need to Worry ? (thanks Kent)

- Consult beam physicists: they should know what the bunch phase jitter is and whether there is a large 1/f component
- If the phase jitter is large for us to worry about, can measure its effect on the BCMs by comparing cavities tuned to different harmonics of the bunch frequency

$$\sigma(\phi_{\rm BCM}) = 2\pi f_{\rm cavity} \sigma(t_{\rm bunch}) = \frac{f_{\rm cavity}}{f_{\rm acc}} \sigma(\phi_{\rm bunch})$$

- E.g. build a pair of cavities tuned to 4th harmonic, 998 MHz.
- They should not be that large, and can be anywhere in A-line